Learning precise 3D reaching in a humanoid robot

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Abstract— In this paper we discuss the implementation of a precise reaching controller on an upper-torso humanoid robot. The proposed solution is based on a learning strategy which does not rely on *a priori* models of the kinematics of the arm nor of that of the head. After learning, the robot can reach for visually identified objects in 3-D space by integrating an open loop and a closed loop component; the open loop controller allows ballistic movements, while the closed loop one performs precise positioning of the hand in visual space. Differently from other approaches we handle the critical case of redundancy in the head and the arm and propose a solution that although preliminary possesses some biological relevance.

Index Terms— Visual servoing, reaching, learning, development, humanoid robotics.

I. INTRODUCTION

Growing evidence in developmental psychology shows the importance of motor activity for cognitive development in humans [1]. In particular it is through manipulation that infants gain direct access to objects and discover properties that otherwise would remain hidden. This concerns for example properties like weight, shape, texture and softness that are, if not impossible, at least extremely hard to perceive by using visual information alone. In adults information originating from motor activity and direct contact with the environment, supports perception [2]; during development the physical interaction with the environment provides infants with natural invariances that are useful occasions for learning. Interestingly, motor and perceptual development seem to follow synchronous schedules as if new achievements in the motor system were promoting the development of new perceptual skills [3].

Research in developmental robotics has demonstrated the importance of motor activity (in particular manipulation) for visual and haptic perception [4]. One of the limitations of these approaches is that controlling the interaction between the robot and the environment is difficult especially when precise models are not available. Experiments with robots have thus focused on situations in which the interaction with objects is relatively simple. For these reasons the investigation of perceptual development in robots requires addressing the problem of motor development first.

In this context we focus on reaching, which is a clear prerequisite for manipulation. Reaching can be solved either by visual servoing [5] or by a model-based open loop [6], Giorgio Metta

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[7] approach. Visual servoing requires the simultaneous view of the hand and of the target and it is limited by the rate of measurement of these two quantities from images. Visual servoing *en force* of the feedback loop is robust to noise and errors guaranteeing convergence to the target even in the presence of rough estimates of the controller parameters (typically a visuo-arm Jacobian). On the contrary, an open loop controller can be as fast as the motors can be at the price of precision which is bound to the modeling inaccuracies or sensor noise.

Results in developmental psychology suggest that both solutions might be adopted by the brain. Clifton et al. [8] tested whether infants require vision of their hand when reaching; they found that infants' ability to touch (and grasp) objects is independent of whether sight of the hand is available or not. Another set of experiments [9] show that later on in development there is an increase of visual guidance in reaching. Together these results suggest the hypothesis that there are two "distinct" reaching mechanism: one that relies on "proprioceptive" information alone and one that uses "visual feedback" to compensate for errors in the visual domain. There are studies that show the link of the control of the gaze in relation to the precision of reaching [10]. In this paper we integrate the two modes of control with an approach based on the hypothesis that the target object is fixated. We use the open loop controller to bring the hand close to the target. The closed loop controller is activated when visual feedback from the hand is available. In practice, we show that the error could be made arbitrarily small. The problem of redundancy is solved in the first case by imposing additional constraints on the task. Finally, we describe the procedure by which the robot learns all the transformations required by the controllers (the open-loop mapping and the arm visual Jacobian).

II. PREVIOUS WORKS

In this section we briefly describe previous approaches to the problem of learning how to reach visual targets with a robot arm. In the literature the problem is often split into two components, open loop and closed loop.

The *open loop* phase requires a sensory-motor map encoding the relationship between the hand visual location and the arm position. Following a classical procedure, this map can be decomposed into three parts: the robot forward kinematics (mapping the hand reference frame into a reference frame on the robot), the camera projective map (mapping the hand reference frame into a camera reference frame) and the hand/eye map (mapping the camera reference frame) and the hand reference frame). Extensive literature is available describing different calibration procedures for retrieving each of these basic maps. Suitable kinematic [11] and hand/eye [12] calibration procedures can be used to retrieve the forward kinematics and the hand/eye maps. Similarly, different algorithms and strategies have been proposed for cameras and stereo rigs calibration, a well known problem in itself, studied mainly in computer vision [13].

Although the final result of these procedures can be extremely accurate, the standard calibration techniques require the robot to operate in a highly structured environment (typically represented by a calibrated grid or a known object) with a precisely calibrated hand pose sensor (typically a stereo rig), which is not desirable in certain applications. Alternative procedures have been proposed in order to relax some of the above assumptions. In [14] for example, an hand/eye calibration procedure which does not use a calibration object is proposed. Other approaches have introduced the possibility of performing a kinematic calibration without measuring the hand pose [15] by relying on proprioception and specific kinematic constraints (e.g. by keeping the hand stationary with respect to the ground, used as reference).

For certain applications the classical calibration procedures are not necessary. A simpler approach [6] avoids the estimation of the three maps mentioned above by learning a single forward map. In this case the map links the head joint position to the corresponding arm position while maintaining the hand at the center of the images (fixation). When the robot fixates the target reaching can be performed by inverting this map to retrieve the arm command which brings the hand to the fixation point. Recently this approach has been successfully extended to redundant manipulators [16], although in the case of a 2-dimensional visual space.

The *closed loop* controller requires knowledge of the Jacobian of the open loop map. It can be derived analytically from mathematical differentiation of the function describing the forward map itself. Alternatively, some techniques directly estimate the Jacobian matrix [17], [18] or its inverse [19].

In this paper we integrated together the open [6], [18], [20] and closed [16], [17] loop strategies, both performed in the 3-dimensional space. We also propose a procedure to estimate the Jacobian of the manipulator in the case of a redundant head and arm. All the transformations required to perform the task, are autonomously estimated by the robot without relying on any *a priori* knowledge about the robot kinematic structure and without an explicit manual labeling of the training data.



Fig. 1. The humanoid robot James.

III. THE ROBOTIC SETUP

The experiments described in this paper were carried out on the robot James (see figure 1 and [21] for more details). James is an upper body humanoid robot which consists of 22 DOFs, actuated by a total of 23 motors. Torque is transmitted to the joints by belts and stainless-steel tendons. The head is equipped with two eyes, which can pan and tilt independently (4 DOFs), and is mounted on a 3-DOF neck. The arm has 7 DOFs: three of them are located in the shoulder, one in the elbow and three in the wrist. The hand has five fingers and is under-actuated with a total of 20 degrees of freedom controlled by 8 motors.

The head structure has a total of 7 degrees of freedom, actuated by 8 motors. Four of these motors are used to independently actuate the pan and tilt movements of the left and right eyes. To achieve a more human-like motion our strategy was to couple the movements of the eyes. We used common tilt α_t^c , vergence α_v^d and version α_v^c . The neck has three degrees of freedom, denoted θ_y , θ_p and θ_r for yaw, pitch and roll respectively.

To summarize, the variables relevant to understand the remainder of the paper are: the head joints $\mathbf{q}_{head} = \left[\alpha_t^c \ \alpha_v^d \ \alpha_v^c \ \theta_y \ \theta_p \ \theta_r\right]^\top \in \mathbb{R}^6$ and the first four arm joints (3 d.o.f. shoulder and elbow) denoted $\mathbf{q}_{arm} \in \mathbb{R}^4$.

IV. GAZE CONTROL

The crucial aspect in the control of gaze concerns the redundancy of the head. Let u_r and v_r be the coordinates of the target on the right image plane. Similarly, let u_l and v_l be the coordinates of the target on the left image plane (see Figure 2). The values of u_r , v_r , u_l , v_l are the output of a visual module which detects the target in the image planes. Directing gaze toward the target consists in moving the neck and the eyes so as to obtain $u_r = 0$, $v_r = 0$, $u_l = 0$, $v_l = 0$. Let us define the vector $\tilde{\mathbf{u}}_{target} = \begin{bmatrix} u_r & v_r & u_l & v_l \end{bmatrix}^\top \in \mathbb{R}^4$ corresponding to the target location in the image planes. Under reasonable assumptions, we do not need to impose simultaneously the four conditions $u_r = 0$, $v_r = 0$, $u_l = 0$, $u_l = 0$, $v_l = 0$. Our control task can be redefined as the problem of controlling $\mathbf{u}_{target} = \begin{bmatrix} u_r & u_l & v_l \end{bmatrix}^\top \in \mathbb{R}^3$ to zero. Clearly, the task specification does not constrain all the head degrees



Fig. 2. Two typical images taken from the cameras mounted on the eyes of the robot (resolution 320×240). The coordinates of the target (the blue ball) on the image planes will be denoted u_l , v_l , and u_r , v_r (respectively left and right cameras).

of freedom (we are imposing 3 constraints but we have 6 free variables available). We solve this "redundancy problem" by using two controllers for the eyes and the neck. The former controls the eyes version and common tilt to track the object, while the latter controls neck yaw and pitch to maintain the eyes "centered" within the neck. Mathematically the above strategy can be implemented as follows:

$$\begin{cases} \dot{\alpha}_v^c = K_p(u_l + u_r) \\ \dot{\theta}_y = K_y \alpha_v^c \end{cases}, \quad \begin{cases} \dot{\alpha}_t^c = K_t(v_l + v_r) \\ \dot{\theta}_p = K_r \alpha_t^c \end{cases}, \quad (1)$$

where α_v^c and α_t^c are the eyes tilt and common version and where θ_y and θ_p are the yaw and pitch movement of the neck. In the proposed control scheme, the vergence degree of freedom α_v^d , which corresponds to the distance of the target does not influence the neck position and is therefore controlled separately from the neck:

$$\alpha_v^d = K_p(u_l - u_r). \tag{2}$$

Finally, the neck roll degree of freedom θ_r is maintained fixed, i.e. $\theta_r^d = 0$.

The proposed control strategy allows us to asymptotically fixate the target $(u_l \rightarrow 0, v_l \rightarrow 0, u_r \rightarrow 0$ which implies $v_r \rightarrow 0$) while, at least within the mechanical limits of the head, also guaranteeing a straight gaze $(\alpha_v^c \rightarrow 0, \alpha_t^c \rightarrow 0)$.

V. REACHING

In this section, we describe the two approaches we followed to solve the reaching task on our robot. The first method uses the forward mapping between the arm joint space and the three dimensional position of the hand represented in the head reference frame. The second method uses a visual servoing technique to control the speed of the arm to minimize the position of the hand in the image plane with respect to a desired target (the fixated object).

A. Open Loop Reaching

Suppose that the robot is tracking a target as described in Section IV. In the assumption of perfect tracking (the visual error is zero), the three dimensional spatial position of the target with respect to the robot, denoted $\tilde{\mathbf{x}}_{target} \in$

 \mathbb{R}^3 , is a function of the head configuration $\mathbf{q}_{head} =$ $\begin{bmatrix} \theta_y & \theta_p & \theta_r & \alpha_v^d & \alpha_v^c & \alpha_t^c \end{bmatrix}^\top \in \mathbb{R}^6.$ However, the representation of the target position, $\tilde{\mathbf{x}}_{target}$, in terms of the full head configuration, q_{head} , is redundant. Specifically, the same target position can be represented by different head configurations. To obtain a one to one mapping between the target position and the head configuration we have to analyze the gaze controller. The latter maintains θ_r stationary $(\theta_r^d = 0)$ and poses additional constraints on the head joints. In particular the controller minimizes α_t^c and α_v^c (see equation (1)) so that they converge to zero ($\alpha_t^c \rightarrow 0$ and $\alpha_v^c \to 0$). Ideally, after fixation is achieved, we have $\mathbf{q}_{head} = \begin{bmatrix} \theta_y & \theta_p & 0 & \alpha_v^d & 0 & 0 \end{bmatrix}^\top \in \mathbb{R}^6$. Since there exists a one to one mapping between the three dimensional position of the target $\tilde{\mathbf{x}}_{target}$ and the three non-zero variables $\theta_u, \, \theta_p$ and α_v^d , we can define $\mathbf{x}_{target} = \begin{bmatrix} \theta_y & \theta_p & \alpha_v^d \end{bmatrix}^\top \in \mathbb{R}^3$. This new variable $\mathbf{x}_{target} \in \mathbb{R}^3$ uniquely codes the spatial position of the target in a way that resembles a three dimensional polar representation. In particular θ_y and θ_p code *azimuth* and elevation, while distance is substituted with α_v (the vergence angle).

If the robot tracks the hand, the same subset of the head joint space can be used to code the spatial location of the hand: $\mathbf{x}_{hand} = \begin{bmatrix} \theta_y & \theta_p & \alpha_v^d \end{bmatrix}^\top \in \mathbb{R}^3$. Under these assumptions, the *forward mapping* f_{arm} relates the arm configuration \mathbf{q}_{arm} with the position of the hand \mathbf{x}_{hand} :

$$\mathbf{x}_{hand} = f_{arm}(\mathbf{q}_{arm}), \qquad f_{arm} : \mathbb{R}^4 \longrightarrow \mathbb{R}^3.$$
 (3)

In the next section we show how a neural network could be trained to approximate f_{arm} .

Suppose now that the robot is fixating a target and that we want to control the robot to reach for it. Formally the problem can be formulated as determining the value of q_{arm} which solves the following optimization problem:

$$\min_{\mathbf{q}_{arm}} \|\mathbf{x}_{hand} - \mathbf{x}_{target}\|^2, \qquad (4)$$

where \mathbf{x}_{target} is measured from the encoders of the head, while \mathbf{x}_{hand} is computed from \mathbf{q}_{arm} through Eq. (3). Given the redundancy of the arm kinematics this minimization has infinite solutions. We constrained the problem by forcing one of the joints, for example joint number 2 (one of the shoulder joints), to remain as close as possible to a predefined value q_{20} :

$$\min_{\text{Harm}} \left[\| \mathbf{x}_{hand} - \mathbf{x}_{target} \|^2 + (q_{arm,2} - q_{20})^2 \right].$$
(5)

The optimization of (5) can be performed numerically using various algorithms. In our implementation, we used the downhill simplex method [22].

B. Learning the open loop reaching

To learn the forward map of Eq. (3) we programmed the robot to perform random movements with the arm (chosen to uniformly sample a predefined region in the robot workspace). During this "exploratory" phase the robot tracked the hand, and collected samples of the form: $\left(\mathbf{q}_{arm}^{i}, \mathbf{x}_{hand}^{i} \right)_{i=0,1...}$ A neural network was then trained to learn the relation:

$$\mathbf{x}_{hand} = \hat{f}_{arm} \left(\mathbf{q}_{arm} \right), \tag{6}$$

which approximates Eq. (3).

In the experiment reported in this paper we collected a data set of about 2890 samples that we divided in a training set ($N_{train} = 2168$ samples) and a test set ($N_{test} = 725$ samples). The neural network we employed was the Receptive Field Weighted Regression model proposed by [23]. This network implements an online learning method, meaning that a learning step is performed every time a new sample is presented to the network. All samples in the training set were shown to the network in a random order. After each training step the performance of the network was validated on the whole test set, by computing the Mean Squared Error (*MSE*) between each sample in the test set, and the corresponding network output.

The plot in figure 3 shows the trend of the error on the test set during learning. At the end of the training the network reached the performance of $MSE = 5.7 \ deg^2$ (with $STD = 10.4 \ deg^2$).

In the experiment reported in this paper the network was trained offline. This was done to simplify the analysis of the results and to perform cross-validation on a predefined test set. However, the learning algorithm we used is purely incremental (each sample was shown to the network only once and immediately discarded), so in this regard it would be straightforward to convert the same approach to an online implementation.

C. Closed Loop Reaching

If the robot could visually measure the distance between the hand and the target, reaching could also be solved visually by implementing a closed control loop. This consists in performing a preliminary (open loop) reaching movement and then refining the action by visually correcting any residual error.

We know that the Jacobian matrix relates arm velocities $\dot{\mathbf{q}}_{arm}$ with hand velocities in the image plane $\dot{\mathbf{u}}_{hand} = \begin{bmatrix} \dot{u}_r & \dot{u}_l & \dot{v}_l \end{bmatrix}^{\top}$:

$$\dot{\mathbf{u}}_{hand} = \mathbf{J} \left(\mathbf{q}_{arm}, \mathbf{q}_{head} \right) \dot{\mathbf{q}}_{arm},\tag{7}$$

where $\tilde{\mathbf{J}} \in \mathbb{R}^{3 \times 4}$ depends on both the configuration of the arm and the head. In practice, assuming sufficiently small arm movements $\Delta \mathbf{q}_{arm}$, we can use the following approximation:

$$\Delta \mathbf{u}_{hand} = \mathbf{J} \left(\mathbf{q}_{arm}, \mathbf{q}_{head} \right) \Delta \mathbf{q}_{arm},\tag{8}$$

where $\Delta \mathbf{u}_{hand}$ is the image plane displacement resulting from the arm movement $\Delta \mathbf{q}_{arm}$. Due to the additional constraints



Fig. 3. Left: learning of the arm forward function. Right: learning the arm jacobian. The plots represent the *MSE* on the test set during learning. See text for more details

posed by the head tracker, we showed that only a subset of \mathbf{q}_{head} , \mathbf{x}_{target} , is sufficient to uniquely identify the position of the head, so we can rewrite equation (8) as:

$$\Delta \mathbf{u}_{hand} = \tilde{\mathbf{J}} \left(\mathbf{q}_{arm}, \mathbf{x}_{target} \right) \Delta \mathbf{q}_{arm}, \qquad \tilde{\mathbf{J}} \in \mathbb{R}^{3 \times 4}.$$
(9)

Moreover, after the preliminary open loop reaching movement, we know that $\mathbf{x}_{target} = f_{arm}(\mathbf{q}_{arm})$ so that Eq. (9) can be further simplified to:

$$\Delta \mathbf{u}_{hand} = \mathbf{J} \left(\mathbf{q}_{arm} \right) \Delta \mathbf{q}_{arm}, \qquad \mathbf{J} \in \mathbb{R}^{3 \times 4} \qquad (10)$$

where **J** depends only on the arm joint configuration q_{arm} .

Suppose now that the robot has to reach for an object, whose visual position is represented by \mathbf{u}_{target} . To solve this problem the controller of the arm needs to compute the arm command which minimizes the error $e = \|\mathbf{u}_{hand} - \mathbf{u}_{target}\|^2$. When the head tracker has achieved convergence on the object, $\mathbf{u}_{target} \approx 0$ and $e \approx \|\mathbf{u}_{hand}\|^2$. Due to the redundancy of the arm, the minimization of e can have infinite solutions. Among them, the minimum norm solution corresponds to the minimum joint speeds, that is:

$$\dot{\mathbf{q}}_{arm} = -k \cdot \mathbf{J}^{\#} \mathbf{u}_{hand}, \qquad \mathbf{J}^{\#} \in \mathbb{R}^{4 \times 3}, \qquad (11)$$

where $\mathbf{J}^{\#}$ is the Moore-Penrose pseudo-inverse of \mathbf{J} . In practice $\mathbf{x}_{target} = f_{arm}(\mathbf{q}_{arm})$ is estimated through Eq. 6, so only an approximated value $\hat{\mathbf{J}}^{\#}$ will be available. Convergence is guaranteed if $\hat{\mathbf{J}}^{\#} \cdot \mathbf{J} > 0$ [24].

D. Learning the Arm Jacobian

As described in Section V-B, the robot moves the arm randomly, while maintaining gaze on the hand. At the end of each movement j the arm is in a configuration \mathbf{q}_{arm}^{j} , while the eyes are fixating the hand ($\mathbf{u}_{hand} \approx 0$). Each arm configuration corresponds to a different value of $\mathbf{J}_{j} = \mathbf{J} (\mathbf{q}_{arm}^{j})$. Now the robot inhibits the head tracker and performs a sequence m of small arm movements $\Delta \mathbf{q}_{arm}^{k}$ which perturb \mathbf{u}_{hand} of small amounts $\Delta \mathbf{u}_{hand}^{k}$: ($\Delta \mathbf{u}_{hand}^{k}, \Delta \mathbf{q}_{arm}^{k}$)_{k=0,1...,m}. All m perturbations $\Delta \mathbf{u}_{hand}^{k}$ and $\Delta \mathbf{q}_{arm}^{k}$ are linearly related through \mathbf{J}_{i} as described in Eq. (9). From these m observations we can derive a least squares estimation of \mathbf{J}_{j} from which, in turn, we can compute the pseudo-inverse $\mathbf{J}_{i}^{\#}$.



Fig. 4. Open loop performance, for different choices of the redundant variable q_{20} (image plane errors \mathbf{u}_{hand} , in pixels). On the horizontal axis u_r and u_l ; vertical axis v_r and v_l (always in pixels). The hand position in the image plane is represented by the small circles. Each circle corresponds to a different open loop movement, i.e. a different value of q_{20} .



Fig. 5. Traces of different closed loop control actions. Each trace correspond to a different Cartesian position of the target to be reached (which is always at the center of the image planes). All the traces end up in the image center thus indicating that the visual errors are completely eliminated by the closed loop controller.

Re-iterating this procedure leads to the collection of a series of examples: $\left(\mathbf{q}_{arm}^{j}, \mathbf{J}_{j}^{\#}\right)_{j=0,1...}$. An approximation $\hat{\mathbf{J}}^{\#}$ of $\mathbf{J}^{\#}$ is finally obtained by training a neural network:

$$\mathbf{g}(\mathbf{q}_{arm}), \qquad g: \mathbb{R}^4 \longrightarrow \mathbb{R}^{12},$$
 (12)

whose output components are the coefficients of $\hat{\mathbf{J}}^{\#} \in \mathbb{R}^{4 \times 3}$.

We report here the result of a learning session. The robot explored 210 different arm positions \mathbf{q}_{arm}^{j} randomly distributed within a region of the workspace. In each of these positions the robot executed m = 10 perturbations $\Delta \mathbf{q}_{arm}^{k}$ and estimated an example $\mathbf{J}_{j}^{\#}$ for the neural network. Overall we collected 210 samples for $\mathbf{J}^{\#}$. We trained the neural network on a subset of $N_{train} = 158$ elements (training set); each sample was shown to the network only once and then discarded. Following each training step, we evaluated the performance of the network by computing MSE on the remaining $N_{test} = 52$ elements (test set). At the end of the training the error on the test set was $MSE = 2 \frac{pixels^2}{deg^2}$ ($STD = 7.1 \frac{pixels^2}{deg^2}$). Figure 3 reports the plot of the error during learning.

VI. RESULTS

In this section we report the results of the experiments we carried out to quantify the performance of the reaching movements. Following the proposed strategy, in order to reach for the target we first need to fixate it, i.e. $\mathbf{u}_{target} = 0$.



Fig. 6. Movement of the hand on the image planes (320×240) during the execution of different reaching actions. Solid line: closed loop. Dashed trace: open loop. Clearly the open loop movement drives the hand to the target (the image centers) with a relatively small error. The closed loop phase reduces this error to zero.



Fig. 7. Time response of the closed loop and open loop strategy. Solid lines: u_r and u_l . Dashed lines: v_r and v_l . Remarkably, the open loop phase is faster but does not drive the hand exactly on the target. The closed loop is slower but more accurate.

Using the available sensor (i.e. vision) the best we can do to precisely reach the target is moving the hand to the fixation point, i.e. $\mathbf{u}_{hand} \longrightarrow 0$. Clearly, the image plane distance $e = \|\mathbf{u}_{hand} - \mathbf{u}_{target}\|$ can be used as a rough estimate of the reaching precision, i.e. of the Cartesian distance between the target to be reached and the position of the hand.

The first attempt to reach the target consists in using (5) to choose the arm configuration \mathbf{q}_{arm} which brings the hand to the center of the image planes. Clearly, if the forward kinematic function (3) were perfectly represented and if the target were reachable, then we would have $\mathbf{x}_{hand} = \mathbf{x}_{target}$, which implies that the target-hand Cartesian distance is zero, e = 0 (see Section V for details). In practice, the model (3) cannot exactly represent the system's kinematics , therefore it is not guaranteed that after the movement execution e = 0. Figure 4 shows the image plane errors after the execution of the open loop movement. The plot has been obtained by fixating a target and performing a series of open loop movements. Each open loop movement was different because (5) was solved by choosing a different value q_{20} .

The residual image plane errors can be reduced by a visual closed loop control strategy. This control strategy moves the arm to progressively drive the hand position in the image planes (\mathbf{u}_{hand}) to zero. Figures 5, 6 and 7 show how the hand is actually driven to the exact image center in both the image planes. The closed loop controller improves the accuracy of the reaching movement, but at the cost of a slower execution speed (see Figure 7). Moreover, it is important to notice the quasi-linearity of the path followed by the hand (see Figure

5). This linearity denotes a good accuracy of the learned Jacobian.

VII. CONCLUSIONS

In this paper we have described the implementation of a reaching behavior that integrates together an open loop and a closed loop controller. The open loop controller allows the robot to perform faster movements and does not require visual feedback from the hand. When sight of the hand is available the closed loop controller allows for precise positioning of the hand in the image plane.

We describe an exploration strategy by means of which the robot autonomously acquires the forward motor map and the visual Jacobian transformations. Among other things this strategy allows the estimation of the eye-to-hand visual Jacobian of the robot. The estimation of the Jacobian is a well studied task for which several solutions have been proposed [17]–[19]. None of these works, however, address the problem of the redundancy of both the head and the arm. In the experiments reported here the estimation of the Jacobian is performed with good accuracy for a subset of the arm workspace and for *different head postures*. We believe this is an important contribution with respect to the state of the art.

We do not rely on prior information about the kinematic structure of the robot. The only major simplification was that we used a color marker to visually localize the hand of the robot. Our assumption is that the hand localization/identification is a separate problem that needs to be solved before learning to reach. Previous work have suggested procedures by which the robot could autonomously learn to solve this task [25], [26]. It will be interesting to see how these approaches can be integrated with the work described in this paper.

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